2007 Aircraft Structural Integrity Program Conference

The Effect of Stress Intensity Factor Models on Inspection Intervals



AIR FORCE

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Integrity - Service - Excellence

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- K Solutions
 - Geometric & Loading Parameter Space
 - [°] Verification
 - Validation
- Fatigue Life Predictions Using New K Solutions
 - [°] Fatigue Life
 - Continuing Damage Scenario
 - > Phase I Life
 - › Crack Size
 - ° Effect of r/t
- Conclusions

Small differences in *K* Solutions yield large cumulative differences in fatigue life

... and large differences in K solutions yield even a larger cumulative difference in fatigue life



Parameter Space

K-Solutions, ≈ 1.0 million CPU Hours

- Geometry
 - Centrally Located Straight Shank Hole
 - $^{\circ} \quad 0.1 \leq r/t \leq 10.0$
 - 0.1, 0.111, 0.125, 0.1428, 0.1667, 0.2,
 0.25, 0.333, 0.5, 0.667, 0.75, 0.8, 1.0,
 1.25, 1.333, 1.5, 1.667 2.0, 3.0, 4.0, 5.0,
 6.0, 7.0, 8.0, 9.0, 10.0 (r/t = 0.5, 1.0)
 - ° Finite Width/Height Plate
 - → r/h = 0.0025
 - → r/b = 0.0025
- Crack Shapes
 - $^{\circ} \quad 0.1 \leq a/c \leq 10.0$
 - > 0.1, 0.111, 0.125, 0.1428, 0.1667, 0.2, 0.25, 0.333, 0.5, 0.667, 0.75, 0.8, 1.0, 1.25, 1.333, 1.5, 2.0, 3.0, 4.0, 5.0, 6.0, 7.0, 8.0, 9.0, 10.0 (a/c = 0.2, 0.5, 0.8, 1.0, 2.0)
 - $^{\circ} \quad 0.1 \leq a/t \leq 0.99$
- Load Conditions
 - Tension
 - ° Bending
 - Pin Loading (Bearing)
- <u>5,672,700</u> solutions





K-Solution Verification



Convergence: Shallow Crack





Convergence: Deep Crack



K-Solution Validation







Marker Load Spectrum









Crack Shape Development





Crack Shape Development





Crack Shape Development



Fatigue Life Predictions Using New K Solutions

Geometry for Assessing Effect on Life $\frac{Small Crack - Thin Sheet}{W = 1.14 in, t = 0.063 in, D = 3/16 in} \\ a_i = 0.01 in, c_i = 0.01 in, a_i/t = 0.2 \\ a_i/c_i = 1.0, r/t = 1.5 \\ TSR = 1.0, BSR = 0.4 \\ \frac{Small Crack - Thick Sheet}{W = 4.53 in, t = 0.25 in, D = \frac{3}{4} in}$



a_i/*c_i* = 1.0, *r*/*t* = 1.5

TSR = 1.0, *BSR* = 0.4 Large Crack – Thin Sheet

W = 1.14 in, t = 0.063 in, D = 3/16 in $a_i = 0.05$ in, $c_i = 0.05$ in, $a_i / t = 0.8$ $a_i / c_i = 1.0$, r/t = 1.5TSR = 1.0, BSR = 0.4

2r $\sigma_{bending}$ σ_{o} $\boldsymbol{a}_{\scriptscriptstyle 1}$ **a**,



Effect on Life – Small Crack, Thin Sheet





Effect on Life – Small Crack, Thick Sheet





Effect on Life – Large Crack, Thin Sheet





 $\sigma_{_{O}}$





Effect on Continuing Damage Scenario Phase I Life





Effect on Continuing Damage Scenario Phase I Crack Length





Effect of *r/t* – Symmetric Corner Cracks





Effect of *r/t* – Single Corner Crack





- Verification
 - *hp*-version FEA + Splitting Scheme = Accurate K-Solutions
- Validation
 - [°] Fatigue life predictions are slightly conservative
- 5,672,700 K solutions for unsymmetric corner cracks at a hole subject to tension, bending, bearing
 - Solutions available in tabular form currently in AFGROW
 - > 75 1.5MB ASCII files
 - Source code for multi-dimensional interpolation also available



- Single vs. Double Cracks
 - ^o Difference always larger for single cracks
- Effect on Fatigue Life
 - Small cracks in thin sheets: 20-50%
 - Small cracks in thick sheets: 25-45%
 - Large cracks in thin sheets: 90-300%
 - Continuing damage scenario: 125-350%
- Effect on Inspections
 - [°] Possibility of initial inspection not early enough in aircraft life
 - Possibility of recurring inspections not occurring as frequently as required
- Effect of *r/t*
 - Significant for large cracks in thin sheets
 - Negligible for small cracks in thick sheets